

Appendix 3-1

Calculation of Odour Emission Rate

Appendix 3.1 Calculation of Odour Emission Rate (Unmitigated)

Facilities No.	Source	Emission Factors	Parameters	
1	Odour Control Unit 1 (MIT) (OD1 & OD2) Both OD1 & OD2 are designed for all below facilities, thus each emission rate would be half of the total emission	Unmitigated OU/s (one control unit)	8.93973E+02 Total flow rate of each vent pipe (m ³ /s) Emission Height, (m) Diameter of the stack, (m) Stack velocity, (m/s) Mitigation %	7.75 <i>from Engineer</i> 6.58 <i>from Engineer</i> 1.0 <i>from Engineer</i> 9.87 <i>calculated</i> 90
	Enclosed Facilities: Solids Handling Building	OU/s	3.4971E+03 Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Air volume of the emission source, A (m3) Total Exposed Area (m2) Ventilation rate, V (air changes per hour) Correction factor, Ct	E = DF x A x (V/3600) x Ct 6595 <i>from HATS2A</i> 97 <i>assumed (1*Surface Area)</i> 97 <i>from Engineer</i> 15 <i>from Engineer</i> 1.31 <i>Temperature correction factor</i>
	Low Lift and Returns Pumping Station	OU/s	3.0586E+02 Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Temperature of sewage, T (F) Oxidation-reduction potential of sewage, ORP (mV) Air volume of the emission source, A (m3) Total Exposed Area (m2) Ventilation rate, V (air changes per hour)	E = DF x A x (V/3600) 1915 <i>calculated, DF = 1.6 x (T/10)^{4.9} x (ORP + 200)^{-0.59}</i> 86 <i>assumed</i> 150 <i>assumed</i> 115 <i>assumed (1*Surface Area)</i> 115 <i>from Engineer</i> 5 <i>assumed 5 air changes per hour</i>
	Flash Mixing and Flocculation Tanks	OU/s	3.3459E+03 Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Temperature of sewage, T (F) Oxidation-reduction potential of sewage, ORP (mV) Air volume of the emission source, A (m3) Total Exposed Area (m2) Ventilation rate, V (air changes per hour)	E = DF x A x (V/3600) 1915 <i>calculated, DF = 1.6 x (T/10)^{4.9} x (ORP + 200)^{-0.59}</i> 86 <i>assumed</i> 150 <i>assumed</i> 1258 <i>assumed (1*Surface Area)</i> 1258 <i>from Engineer</i> 5 <i>assumed 5 air changes per hour</i>
	Sedimentation Tank (Weir Zone) (PR01)	OU/s	3.6616E+03 Odour Emission Rate at weir (OU/s/m) Odour potential, OP (OU/m3) Weir loading rate, F _{weir} (m3/m/h) Height of drops of liquid flow at weirs, h (m) pH correction coefficient, K _{pH} Surface Area of weir, m2 Weir width per each tank(m) Weir length per each tank (m) Dry Weather Flow in Phase 2 (m3/d) No. of Tanks Mitigation %	E = 7.16 x 10 ⁻⁴ x OP x F _{weir} x h x K _{pH} 3305 <i>from Yang & Hobson</i> 122.45 <i>from Engineer</i> 0.12 <i>from Engineer</i> 1.17 <i>pH=7, from DSD,</i> 225 <i>from Engineer</i> 2.5 <i>from Engineer</i> 10 <i>from Engineer</i> 246000 <i>from DSD</i> 9 0 <i>Odour reduction</i>
	Sedimentation Tank Effluent Channel	OU/s	7.0946E+02 Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Total Surface Area of Sedimentation Tank Effluent Channel, (m2)	E _{ton} = 4 x 10 ⁻³ (0.0103V _{wind} ^{1.42} + 2.93 V _{liquid}) x OP 3305 <i>from Yang & Hobson</i> 8.1331E-02 <i>from Engineer</i> 6.5278E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 225 <i>from Engineer</i>
	Inlet Chamber of Outfall Pumping Station - A	OU/s	3.9039E+02 Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area of Outfall Pumping Station, (m2)	E _{ton} = 4 x 10 ⁻³ (0.0103V _{wind} ^{1.42} + 2.93 V _{liquid}) x OP 3305 <i>from Yang & Hobson</i> 1.1997E-01 <i>from Engineer</i> 1.9444E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 84 <i>from Engineer</i>

Appendix 3.1 Calculation of Odour Emission Rate (Unmitigated)

Facilities No.	Source	Emission Factors	Parameters	
	Inlet Chamber of Outfall Pumping Station - B	OU/s 2.8602E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area of Outfall Pumping Station, (m2)	$E_{ton} = 4 \times 10^{-3} (0.0103 V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 1.1997E-01 <i>from Engineer</i> 2.5139E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 62 <i>from Engineer</i>
	Screw Pumps of Outfall Pumping Station	OU/s 9.3546E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area of Outfall Pumping Station, (m2)	$E_{ton} = 4 \times 10^{-3} (0.0103 V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 1.1997E-01 <i>from Engineer</i> 2.0556E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 201 <i>from Engineer</i>
	Wet Well of Outfall Pumping Station	OU/s 1.6593E+03	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area of Outfall Pumping Station, (m2)	$E_{ton} = 4 \times 10^{-3} (0.0103 V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 1.1997E-01 <i>from Engineer</i> 2.9167E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 357 <i>from Engineer</i>
	Inlet Chamber/Influent Channel, (IN01 - IN04) Screw Pumps, Wet Wells of Inlet Pumping Station	OU/s 1.0105E+03	Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Temperature of sewage, T (F) Oxidation-reduction potential of sewage, ORP (mV) Air volume of the emission source, A (m3) Total Exposed Area of Inlet Pumping Station (m2) Ventilation rate, V (air changes per hour)	$E = DF \times A \times (V/3600)$ 1915 <i>calculated, DF = 1.6 x (T/10)^{4.9} x (ORP + 200)^{-0.59}</i> 86 <i>assumed</i> 150 <i>assumed</i> 380 <i>screw pump:(0.2 (the freeboard) * Surface Area); the other facilities assumed (1*Surface Area)</i> 581 <i>from Engineer</i> 5 <i>assumed 5 air changes per hour</i>
	Coarse Screens and Common Flow Channel (SC01 - SC04)	OU/s 5.7449E+02	Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Temperature of sewage, T (F) Oxidation-reduction potential of sewage, ORP (mV) Air volume of the emission source, A (m3) Total Exposed Area (m2) Ventilation rate, V (air changes per hour)	$E = DF \times A \times (V/3600)$ 1915 <i>calculated, DF = 1.6 x (T/10)^{4.9} x (ORP + 200)^{-0.59}</i> 86 <i>assumed</i> 150 <i>assumed</i> 216 <i>assumed (1*Surface Area)</i> 216 <i>from Engineer</i> 5 <i>assumed 5 air changes per hour</i>
	Aerated Grit Channel and Common Flow Channel (GR01)	OU/s 9.1626E+02	Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Temperature of sewage, T (F) Oxidation-reduction potential of sewage, ORP (mV) Air volume of the emission source, A (m3) Total Exposed Area (m2) Ventilation rate, V (air changes per hour)	$E = DF \times A \times (V/3600)$ 1915 <i>calculated, DF = 1.6 x (T/10)^{4.9} x (ORP + 200)^{-0.59}</i> 86 <i>assumed</i> 150 <i>assumed</i> 345 <i>assumed (1*Surface Area)</i> 345 <i>from Engineer</i> 5 <i>assumed 5 air changes per hour</i>
	Fine Screen and Common Flow Channel after Fine Screens (FSC01 - FSC06)	OU/s 5.8713E+02	Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Temperature of sewage, T (F) Oxidation-reduction potential of sewage, ORP (mV) Air volume of the emission source, A (m3) Total Exposed Area (m2) Ventilation rate, V (air changes per hour)	$E = DF \times A \times (V/3600)$ 1915 <i>calculated, DF = 1.6 x (T/10)^{4.9} x (ORP + 200)^{-0.59}</i> 86 <i>assumed</i> 150 <i>assumed</i> 221 <i>assumed (1*Surface Area)</i> 221 <i>from Engineer</i> 5 <i>assumed 5 air changes per hour</i>

Appendix 3.1 Calculation of Odour Emission Rate (Unmitigated)

Facilities No.	Source	Emission Factors	Parameters		
2	Sedimentation Tanks (Quiescent Zone) (PR02)	Unmitigated OU/s/m2 2.0651E-02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s)		
		OLD 1.8990E-02 (max. rate)			
		OU/s/m2 For surface roughness Zo = 1.0m			
		E_{quiescent zone} class A 1.8904E-02	Wind Speed at emission source, V _{wind-A} (m/s)		
		E_{quiescent zone} class B 1.8956E-02	Wind Speed at emission source, V _{wind-B} (m/s)		
		E_{quiescent zone} class C 1.8990E-02	Wind Speed at emission source, V _{wind-C} (m/s)		
		E_{quiescent zone} class D 1.8988E-02	Wind Speed at emission source, V _{wind-D} (m/s)		
		E_{quiescent zone} class E 1.8922E-02	Wind Speed at emission source, V _{wind-E} (m/s)		
		E_{quiescent zone} class F 1.8854E-02	Wind Speed at emission source, V _{wind-F} (m/s)		
			Friction velocity, U _A * (m/s) Friction velocity, U _B * (m/s) Friction velocity, U _C * (m/s) Friction velocity, U _D * (m/s) Friction velocity, U _E * (m/s) Friction velocity, U _F * (m/s)		
			Mean Obukov length, L _A (m) Mean Obukov length, L _B (m) Mean Obukov length, L _C (m) Mean Obukov length, L _D (m) Mean Obukov length, L _E (m) Mean Obukov length, L _F (m)		
			Karman constant, k Z ₁ , (m) Z ₀ , (m)		
			Eton = 4 x 10 ⁻³ (0.0103V _{wind} ^{1.42} + 2.93 V _{liquid}) x OP 3305 from Yang & Hobson 4.8611E-04 from Engineer 4.7917E-02 from Engineer		
			U _z = (U* / k) x [ln(Z ₁ / Z ₀)-ψ _M (Z ₁ /L)+(ψ _M (Z ₀ /L)] from Komari et al., 5.0559E-03 calculated (for stability class A) 7.3288E-03 calculated (for stability class B) 8.6707E-03 calculated (for stability class C) 8.5910E-03 calculated (for stability class D) 5.9022E-03 calculated (for stability class E) 2.3421E-03 calculated (for stability class F) 2.4129E-01 calculated, (for stability class A) 3.2070E-01 calculated, (for stability class B) 3.6008E-01 calculated, (for stability class C) 3.5399E-01 calculated, (for stability class D) 2.4083E-01 calculated, (for stability class E) 8.8850E-02 calculated, (for stability class F) -1.8357E+01 calculated, (for stability class A) -5.7207E+01 calculated, (for stability class B) -5.0458E+02 calculated, (for stability class C) 1.0000E+08 calculated, (for stability class D) 5.0458E+02 calculated, (for stability class E) 5.7207E+01 calculated, (for stability class F)		
		3	Odour Control Unit (OD3 & OD4) Both OD3 & OD4 deodorized for below facilities, thus each emission rate would be half of the total emission	Unmitigated OU/s (one control unit) 9.39526E+02	Total flow rate of each vent pipe (m ³ /s) Emission Height, (m) Diameter of the stack, (m) Stack velocity, (m/s) Mitigation % Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Ventilation rate, V (air changes per hour) Ventilation rate, V (air changes per hour) Correction factor, Ct
					11.28 from Engineer 6.81 from Engineer 1.0 from Engineer 14.36 calculated 90
					E = DF x A x (V/3600) x Ct 7603 measured max. odour concentration, oum ⁻³ of fresh dewatered sludge at Stonecutter Island STW 5 for Raw Sludge Holding Tanks, Sludge Pumping Station, Return Liqour Pumping Station 15 for Septic Waste Area, Sludge Dewatering Building 1.31 Temperature correction factor
				Septic Waste Area OU/s 6.0756E+02	Air volume of the emission source, A (m3) Total Exposed Area of Septic Waste Area, (m2)
	15 assumed (1*Surface Area) 15 from Engineer				
Raw Sludge Holding Tanks OU/s 1.0043E+04	Air volume of the emission source, A (m3) Total Exposed Area of Raw Sludge Holding Tanks, (m2)				
	726 assumed (1*Surface Area) 726 from Engineer				
Sludge Pumping Station OU/s 4.9800E+02	Air volume of the emission source, A (m3) Total Exposed Area of Sludge Pumping Station, (m2)				
	36 assumed (1*Surface Area) 36 from Engineer				
Return Liqour Pumping Station OU/s 4.1500E+02	Air volume of the emission source, A (m3) Total Exposed Area of Return Liqour Pumping Station, (m2)				
	30 assumed (1*Surface Area) 30 from Engineer				
Sludge Dewatering Building OU/s 3.6453E+03	Air volume of the emission source, A (m3) Total Exposed Area of Sludge Dewatering Building, (m2)				
	88 assumed (1*Surface Area) 88 from Engineer				
Centrifuge OU/s 3.3200E+02	Air volume of the emission source, A (m3) Total Exposed Area of Centrifuge, (m2)				
	24 assumed (1*Surface Area) 24 from Engineer				

Appendix 3.1 Calculation of Odour Emission Rate (Unmitigated)

Facilities No.	Source	Emission Factors	Parameters
	Fine Screens Influent Channel (for disinfection facilities) (FIS01)	OU/s 1.0208E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Exposed Area of Fine Screen Influent Channel (m2)
	Fine Screens (for disinfection facilities) (FIS02-FIS03)	OU/s 2.0164E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Exposed Area of Fine Screen (m2)
	UV Tank Influent Channel (UV01)	OU/s 6.4932E+01	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area (m2)
	UV Tank (UV02-UV03)	OU/s 2.2555E+03	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Exposed Area of UV Tanks (m2)
	UV Tank Effluent Channel (UV04-UV06)	OU/s 6.2551E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Odour Emission Reduction after UV process (%) Exposed Area of UV Effluent Channel (m2)

Note:
 The design wind velocity at the liquid surface of enclosed facilities including sedimentation tank effluent channel; inlet chamber, screw pumps and wet wells of outfall pumping station; fine screens (for disinfection facilities); UV tank influent channel; UV tank & effluent channel would not be greater than 0.00867m/s.

Appendix 3.1 Calculation of Odour Emission Rate (Mitigated)

Facilities No.	Source	Emission Factors		Parameters	
1	Odour Control Unit 1 (MIT) (OD1, OD2 & OD5) Enclosed Facilities no. 2 Both OD1, OD2 & OD5 are designed for all below facilities, thus each emission rate would be one third of the total emission Enclosed Facilities: Inlet Chamber/Influent Channel, (IN01 - IN04) Screw Pumps and Wet Wells of Inlet Pumping Station Coarse Screens and Common Flow Channel (SC01 - SC04) Aerated Grit Channel and Common Flow Channel (GR01) Fine Screen and Common Flow Channel after Fine Screens (FSC01 - FSC06) Solids Handling Building Low Lift and Returns Pumping Station Flash Mixing and Flocculation Tanks Sedimentation Tanks (Quiescent Zone) (PR02) Sedimentation Tank (Weir Zone) (PR01)	Mitigated OU/s (one control unit)	6.0026E+02	Total flow rate of each vent pipe (m ³ /s) Emission Height, (m) Diameter of the stack, (m) Stack velocity, (m/s) Mitigation %	10.86 <i>from Engineer</i> 6.81 <i>from Engineer</i> 1.0 <i>from Engineer</i> 13.82 <i>calculated</i> 90
				Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Temperature of sewage, T (F) Oxidation-reduction potential of sewage, ORP (mV) Ventilation rate, V (air changes per hour) Ventilation rate, V (air changes per hour)	E = DF x A x (V/3600) 1915 <i>calculated, DF = 1.6 x (T/10)^{4.9} x (ORP + 200)^{-0.59}</i> 86 <i>assumed</i> 150 <i>assumed</i> 5 <i>assumed 5 air changes per hour</i> 15 <i>for Solids Handling Building</i>
				Air volume of the emission source, A (m3) Total Exposed Area of Inlet Pumping Station (m2)	380 <i>screw pump:(0.2 (the freeboard) * Surface Area); the other facilities assumed (1*Surface Area)</i> 581 <i>from Engineer</i>
				Air volume of the emission source, A (m3) Total Exposed Area (m2)	216 <i>assumed (1*Surface Area)</i> 216 <i>from Engineer</i>
				Air volume of the emission source, A (m3) Total Exposed Area (m2)	345 <i>assumed (1*Surface Area)</i> 345 <i>from Engineer</i>
				Air volume of the emission source, A (m3) Total Exposed Area (m2)	221 <i>assumed (1*Surface Area)</i> 221 <i>from Engineer</i>
				Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Air volume of the emission source, A (m3) Total Exposed Area (m2) Temperature Correction factor, Ct	E = DF x A x (V/3600) x Ct 6595 <i>from HATS2A measurement data (max odour concentration of screens)</i> 97 <i>assumed (1*Surface Area)</i> 97 <i>from Engineer</i> 1.31 <i>Temperature correction factor</i>
				Air volume of the emission source, A (m3) Total Exposed Area (m2)	115 <i>assumed (1*Surface Area)</i> 115 <i>from Engineer</i>
				Air volume of the emission source, A (m3) Total Exposed Area (m2)	1258 <i>assumed (1*Surface Area)</i> 1258 <i>from Engineer</i>
				Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V _{liquid} (m/s) Wind Velocity, V _{wind} (m/s) Covered Area, (m ²) Mitigation %	E _{ton} = 4 x 10 ⁻³ (0.0103V _{wind} ^{1.42} + 2.93 V _{liquid}) x OP 3305 <i>from Yang & Hobson</i> 4.8611E-04 <i>from Engineer</i> 4.7917E-02 <i>from Engineer</i> 6210 <i>covered all sedimentation tanks</i> 0 <i>Odour reduction</i>
				Odour Emission Rate at weir (OU/s/m) Odour potential, OP (OU/m3) Weir loading rate, F _{weir} (m3/m/h) Height of drops of liquid flow at weirs, h (m) pH correction coefficient, K _{pH} Surface Area of weir, m2 Weir width per each tank(m) Weir length per each tank (m) Dry Weather Flow in Phase 2 (m3/d) No. of Tanks Mitigation %	E = 7.16 x 10 ⁻⁴ x OP x F _{weir} x h x K _{pH} 3305 <i>from Yang & Hobson</i> 122.45 <i>from Engineer</i> 0.12 <i>from Engineer</i> 1.17 <i>pH=7, from DSD,</i> 225 <i>from Engineer</i> 2.5 <i>from Engineer</i> 10 <i>from Engineer</i> 246000 <i>from DSD</i> 9 0 <i>Odour reduction</i>

Appendix 3.1 Calculation of Odour Emission Rate (Mitigated)

Facilities No.	Source	Emission Factors	Parameters	
	Sedimentation Tank Effluent Channel	OU/s 7.0946E+02 7.1053E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Total Surface Area of Sedimentation Tank Effluent Channel, (m ²) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 8.1331E-02 <i>from Engineer</i> 6.5278E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 225 <i>from Engineer</i> 0
	Inlet Chamber of Outfall Pumping Station - A	OU/s 3.9039E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area of Outfall Pumping Station, (m2) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 1.1997E-01 <i>from Engineer</i> 1.9444E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 84 <i>from Engineer</i> 0
	Inlet Chamber of Outfall Pumping Station - B	OU/s 2.8602E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area of Outfall Pumping Station, (m2) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 1.1997E-01 <i>from Engineer</i> 2.5139E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 62 <i>from Engineer</i> 0
	Screw Pumps of Outfall Pumping Station	OU/s 9.3546E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area of Outfall Pumping Station, (m2) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 1.1997E-01 <i>from Engineer</i> 2.0556E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 201 <i>from Engineer</i> 0
	Wet Well of Outfall Pumping Station	OU/s 1.6593E+03	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area of Outfall Pumping Station, (m2) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 1.1997E-01 <i>from Engineer</i> 2.9167E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 357 <i>from Engineer</i> 0
2	Odour Control Unit (mit) (OD3 & OD4) Both OD3 & OD4 deodorized for below facilities, thus each emission rate would be half of the total emission	Mitigated OU/s (one control unit)	Total flow rate of each vent pipe (m ³ /s) Emission Height, (m) Diameter of the stack, (m) Stack velocity, (m/s) Mitigation %	11.28 <i>from Engineer</i> 6.81 <i>from Engineer</i> 1.0 <i>from Engineer</i> 14.36 <i>calculated</i> 90
	Enclosed Facilities: Fine Screens Influent Channel (for disinfection facilities) (FIS01)	OU/s 1.0208E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Exposed Area of Fine Screen Influent Channel (m2) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 8.1331E-02 <i>from Engineer</i> 1.5000E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 32.4 <i>from Engineer</i> 0

Appendix 3.1 Calculation of Odour Emission Rate (Mitigated)

Facilities No.	Source	Emission Factors	Parameters		
	Fine Screens (for disinfection facilities) (FIS02-FIS03)	OU/s	2.0164E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Exposed Area of Fine Screen (m2) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 8.1331E-02 <i>from Engineer</i> 1.1111E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 64 <i>from Engineer</i> 0
	UV Tank Influent Channel (UV01)	OU/s	6.4932E+01	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Total Exposed Area (m2) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 7.6248E-03 <i>from Engineer</i> 5.0556E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 218 <i>from Engineer</i> 0
	UV Tank (UV02-UV03)	OU/s	2.2555E+03	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Exposed Area of UV Tanks (m2) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 7.3198E-02 <i>from Engineer</i> 3.4514E-02 <i>from Engineer</i> 0 <i>from Engineer</i> 795.2 <i>from Engineer</i> 0
	UV Tank Effluent Channel (UV04-UV06)	OU/s	6.2551E+02	Odour Emission Rate (OU/s/m2) Odour potential, OP (OU/m3) Velocity of liquid, V_{liquid} (m/s) Wind Velocity, V_{wind} (m/s) Odour Emission Reduction after UV process (%) Exposed Area of UV Effluent Channel (m2) Mitigation %	$E_{ton} = 4 \times 10^{-3} (0.0103V_{wind}^{1.42} + 2.93 V_{liquid}) \times OP$ 3305 <i>from Yang & Hobson</i> 7.3198E-02 <i>from Engineer</i> 1.0194E-01 <i>from Engineer</i> 0 <i>from Engineer</i> 220.2 <i>from Engineer</i> 0
	Sludge Facilities			Odour Emission Rate (OU/s) Dilution factor, DF (OU/m3) Ventilation rate, V (air changes per hour) Ventilation rate, V (air changes per hour) Temperature Correction factor, Ct	$E = DF \times A \times (V/3600) \times Ct$ 7603 <i>measured max. odour concentration, oum^{-3} of fresh dewatered sludge at Stonecutter Island STW</i> 5 <i>for Raw Sludge Holding Tanks, Sludge Pumping Station, Return Liquor Pumping Station</i> 15 <i>for Septic Waste Area, Sludge Dewatering Building</i> 1.31 <i>Temperature correction factor</i>
	Septic Waste Area	OU/s	6.0756E+02	Air volume of the emission source, A (m3) Total Exposed Area of Septic Waste Area, (m2)	15 <i>assumed (1*Surface Area)</i> 15 <i>from Engineer</i>
	Raw Sludge Holding Tanks	OU/s	1.0043E+04	Air volume of the emission source, A (m3) Total Exposed Area of Raw Sludge Holding Tanks, (m2)	726 <i>assumed (1*Surface Area)</i> 726 <i>from Engineer</i>
	Sludge Pumping Station	OU/s	4.9800E+02	Air volume of the emission source, A (m3) Total Exposed Area of Sludge Pumping Station, (m2)	36 <i>assumed (1*Surface Area)</i> 36 <i>from Engineer</i>
	Return Liquor Pumping Station	OU/s	4.1500E+02	Air volume of the emission source, A (m3) Total Exposed Area of Return Liquor Pumping Station, (m2)	30 <i>assumed (1*Surface Area)</i> 30 <i>from Engineer</i>
	Sludge Dewatering Building	OU/s	3.6453E+03	Air volume of the emission source, A (m3) Total Exposed Area of Sludge Dewatering Building, (m2)	88 <i>assumed (1*Surface Area)</i> 88 <i>from Engineer</i>
	Centrifuge	OU/s	3.3200E+02	Air volume of the emission source, A (m3) Total Exposed Area of Centrifuge, (m2)	24 <i>assumed (1*Surface Area)</i> 24 <i>from Engineer</i>

Note:
 The design wind velocity at the liquid surface of enclosed facilities including sedimentation tank effluent channel; inlet chamber, screw pumps and wet wells of outfall pumping station; sedimentation tanks; fine screens (for disinfection facilities); UV tank influent channel; UV tank & effluent channel would not be greater than 0.00867m/s.